## Directional (Circular) Statistics

Directional or circular distributions are those that have no true zero and any designation of high or low values is arbitrary:

- Compass direction
- Hours of the day
- Months of the year


Time can be converted to an angular measurement using the equation:

$$
a=\frac{\left(360^{0}\right)(X)}{k}
$$

where $a$ is the angular measurement, $X$ is the time period, and $k$ is the number of time units on the circular measurement scale.

What is the angular measurement of 6:15 a.m. (6.25a.m.)?
(Remember to use a 24 hr clock...)

$$
a=\frac{\left(360^{0}\right)(6.25 h r)}{24 h r s}=93.75^{0}
$$

What is the angular measurement of February $14^{\text {th }}$ ?
(Remember to use total days...)

$$
a=\frac{\left(360^{0}\right)(45 \text { th day })}{365 \text { days }}=44.38^{0}
$$

To analyze directional data they must first be transformed into rectangular polar coordinates.

- First, we specify a 'unit circle' that has a radius of 1.
- The polar location is then defined as the angular measurement and its intersection with the unit circle.
- The cosine and sine functions are then used to place this location (based on the angle and unit distance) into a standardized Cartesian space.

$$
\begin{array}{ll}
\cos a=\frac{x}{r} & \sin a=\frac{y}{r} \\
\cos 30=0.50 & \sin 30=0.87 \\
\cos 60=0.50 & \sin 60=0.87
\end{array}
$$

Note that the coordinates of opposite angles are identical. Also note that the $x$ and $y$ axes are opposite of the typical Cartesian plane.



Mean Angle (Azimuth)

The mean angle can not simply be the sum of the angles divided by the sample size, because the mean angle of 3590 and 10 (north) would be 1800 (south)! Therefore we use the following equations:

$$
\begin{aligned}
& Y=\frac{\sum_{i=1}^{n} \sin _{a}}{n} \quad X=\frac{\sum_{i=1}^{n} \cos _{a}}{n} \\
& r=\sqrt{X^{2}+Y^{2}}
\end{aligned}
$$

$$
\cos \bar{a}=\frac{X}{r} \quad \sin \bar{a}=\frac{Y}{r} \quad \theta_{r}=\arctan \left(\frac{\sin \bar{a}}{\cos \bar{a}}\right)
$$

where $X$ and $Y$ are the rectangular coordinates of the mean angle, and $r$ is the mean vector.

## Determining the Quadrant

- Sin + , $\operatorname{Cos}+$ : the mean angle is computed directly.
- $\operatorname{Sin}+$, Cos - : the mean angle $=180-\theta_{r}$
- $\operatorname{Sin}-$, Cos - : the mean angle $=180+\theta_{r}$
- $\operatorname{Sin}-, \operatorname{Cos}+:$ the mean angle $=360-\theta_{r}$.


| Rocks Vectors |  | Sin (Azimuth) | Cos (Azimuth) |
| :---: | :---: | :---: | :---: |
| 341 |  | -0.32557 | 0.94552 |
| 330 |  | -0.50000 | 0.86603 |
| 301 |  | -0.85717 | 0.51504 |
| 299 |  | -0.87462 | 0.48481 |
| 9 |  | 0.15643 | 0.98769 |
| 7 |  | 0.12187 | 0.99255 |
| 359 |  | -0.01745 | 0.99985 |
| 334 |  | -0.43837 | 0.89879 |
| 353 |  | -0.12187 | 0.99255 |
| 15 |  | 0.25882 | 0.96593 |
| 27 |  | 0.45399 | 0.89101 |
| 28 |  | 0.46947 | 0.88295 |
| 25 |  | 0.42262 | 0.90631 |
| 23 |  | 0.39073 | 0.92050 |
| 350 |  | -0.17365 | 0.98481 |
| 30 |  | 0.50000 | 0.86603 |
| 26 |  | 0.43837 | 0.89879 |
| 22 |  | 0.37461 | 0.92718 |
| 8 |  | 0.13917 | 0.99027 |
| 356 |  | $\underline{-0.06976}$ | 0.99756 |
|  | $\Sigma$ | 0.34763 | 17.91415 |

First take the sine and cosine of the angles (azimuths) and sum them.
In Excel the formula is: =sin(radians(cell \#)) and =cos(radians(cell \#)).
$n=20$
$\sum \sin _{a}=0.34763 \quad \sum \cos _{a} 17.91415$
$Y=\frac{0.34763}{20}=0.01738 \quad X=\frac{17.91415}{20}=0.89571$
$r=\sqrt{0.01738^{2}+089571^{2}}=\sqrt{0.00030+0.80229}=0.8959$
$\sin \bar{a}=\frac{0.01738}{0.8959}=0.0194 \quad \cos \bar{a}=\frac{0.89571}{0.8959}=0.9998$
$\theta_{r}=\arctan \left(\frac{0.0194}{0.9998}\right)=1.11 \longleftarrow$ Ignore the sign.

Since the sine is + and the cosine is + , we read the answer directly, regardless of the sign of $\Theta_{r}$. Therefore the angle that corresponds to $\cos (0.9998), \sin (0.0194 \overline{1})$ is $1.11^{\circ} \ldots$ essentially due north.

## Death Valley Rocks Data



The value of $r$ is also a measure of angular dispersion, similar to the standard deviation with a few exceptions:

- Unlike the standard deviation it ranges from 0-1.
- A value of 0 means uniform dispersion.
- A value of 1 means complete concentration in one direction.

$$
r=0
$$



## Bimodal Data

When angular data have opposite azimuths they are said to have diametrically bimodal circular distributions.


The mean angle of diametrically bimodal data is orthogonal (at right angles) to the true mean angle and a poor representation of the data.


One method of dealing with diametrically bimodal circular data is to use a procedure called angle doubling.

Data must be perfectly diametrical for this procedure to work.

## Angle Doubling Procedure:

- Each angle $\left(\mathrm{a}_{\mathrm{i}}\right)$ is doubled (e.g. $34 \times 2=68$ ).
- If the doubled angle is $<3600$ then it is recorded as $2 \mathrm{a}_{\mathrm{i}}$.
- If the doubled angle is $\geq 3600$ then 360 is subtracted from it and the results recorded as $2 \mathrm{a}_{\mathrm{i}}$.
- Then proceed as normal in calculating the mean angle.


## Andean Villages Principal Street Azimuths <br> (labeled slope direction, degrees) <br> Note that these azimuths are not truly unidirectional but are bidirectional.

For example, azimuth 330 has an opposite azimuth of 330-180=150.



Andean Village Subset ( $n=30$ )
Principal Azimuths (diametrically bimodal data)

| Village Azimuth ( $\mathrm{a}_{\mathrm{i}}$ ) | $2 \mathrm{a}_{\text {i }}$ | $\operatorname{Sin}\left(2 a_{i}\right)$ | $\operatorname{Cos}\left(2 a_{i}\right)$ |
| :---: | :---: | :---: | :---: |
| 356 | 352 | -0.1392 | 0.9903 |
| 359 | 358 | -0.0349 | 0.9994 |
| 11 | 22 | 0.3746 | 0.9272 |
| 350 | 340 | -0.3420 | 0.9397 |
| 334 | 308 | -0.7880 | 0.6157 |
| 357 | 354 | -0.1045 | 0.9945 |
| 358 | 356 | -0.0698 | 0.9976 |
| 358 | 356 | -0.0698 | 0.9976 |
| 19 | 38 | 0.6157 | 0.7880 |
| 7 | 14 | 0.2419 | 0.9703 |
| 6 | 12 | 0.2079 | 0.9781 |
| 6 | 12 | 0.2079 | 0.9781 |
| 334 | 308 | -0.7880 | 0.6157 |
| 21 | 42 | 0.6691 | 0.7431 |
| 348 | 336 | -0.4067 | 0.9135 |
| 176 | 352 | -0.1392 | 0.9903 |
| 179 | 358 | -0.0349 | 0.9994 |
| 191 | 22 | 0.3746 | 0.9272 |
| 170 | 340 | -0.3420 | 0.9397 |
| 154 | 308 | -0.7880 | 0.6157 |
| 177 | 354 | -0.1045 | 0.9945 |
| 178 | 356 | -0.0698 | 0.9976 |
| 178 | 356 | -0.0698 | 0.9976 |
| 199 | 38 | 0.6157 | 0.7880 |
| 187 | 14 | 0.2419 | 0.9703 |
| 186 | 12 | 0.2079 | 0.9781 |
| 186 | 12 | 0.2079 | 0.9781 |
| 154 | 308 | -0.7880 | 0.6157 |
| 201 | 42 | 0.6691 | 0.7431 |
| 168 | 336 | -0.4067 | 0.9135 |
|  | $\Sigma$ | -0.8515 | 26.8976 |

$$
\begin{aligned}
& Y=\frac{-0.8515}{30}=-0.0284 \quad X=\frac{26.8976}{30}=0.8966 \\
& r=\sqrt{(-0.0284)^{2}+(0.8966)^{2}}=\sqrt{0.8047}=0.8970 \\
& \cos 2 a_{i}=\frac{0.8966}{0.8970}=0.9996 \\
& \sin 2 a_{i}=\frac{-0.0284}{0.8970}=-0.0317 \\
& \arctan \left(\frac{-0.0317}{0.9996}\right)=-0.0005
\end{aligned}
$$

The mean angle is therefore 360-0.0005 or effectively 360 .

Mean Angle


## Testing the Significance of the Directional Mean

Directional statistics are more sensitive to small sample sizes and it is important to test the directional mean for significance... not something typically done with conventional measures.


Rayleigh z Test

We can use the Rayleigh $z$ test to test the null hypothesis that there is no sample mean direction:
$H_{0}$ : There is no sample mean direction.
$H_{a}$ : There is a sample mean direction.
We determine the Rayleigh z statistic using the equation:

$$
Z=n r^{2}
$$

where $n$ is the sample size and $r$ is taken from the mean angle equation.

The Rayleigh's test has a few very important assumptions:

- The data are not diametrically bidirectional.
- The data are unimodal, meaning there are not more than one clustering of points around the circle.

So for the Andean village azimuth which are diametrically bidirectional we must use the data from the angle doubling procedure.

## From the Andean Village example:

$$
\begin{aligned}
& n=30 \\
& r=0.897 \\
& z=(30)\left(0.897^{2}\right)=24.14 \\
& z_{\text {Critical }}=2.971
\end{aligned}
$$

| n | $\alpha: 0.50$ | 0.20 | 0.10 | 0.0.5 | 0.0.2 | 0.0,1 | 0, 0,05 | 0.0,02 | 0, 0,01 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 0.7.34 | 1.6.39 | 2. 2,74 | 2.8,65 | 3.5,76 | 4.0,58 | 4.4,91 | 4.9,85 | 5. 2.97 |
| 7 | 0.7 .27 | 1.6,34 | 2. 2,78 | 2.885 | 3.6,27 | 4.143 | 4.6,17 | 5.1.81 | 5.5,56 |
| 8 | 0.7 .23 | 1.6.31 | 2. 2.81 | 2.8,99 | 3.6.65 | 4.205 | 4.7,10 | 5.3,22 | 5.7,43 |
| 9 | 0.7.19 | 1.6,28 | 2. 2,83 | 2.9,10 | 3.694 | 4.252 | 4.7 .80 | 5.4,30 | 5.8.85 |
| 10 | 0.7 .17 | 1.6,26 | 2. 2,85 | 2.9,19 | 3.7,16 | 4.289 | 4.8,35 | 5, 5,14 | 5.9,96 |
|  |  |  |  |  |  |  |  |  |  |
| 11 | 0.715 | 1.6,25 | 2. 287 | 2.9,26 | 3.735 | 4.3,19 | 4.8,79 | 5. 5.82 | 6. 0,85 |
| 12 | 0.7 .13 | 1.6.23 | 2. 2,88 | 2.9,32 | 3.7 .50 | 4.3,44 | 4.9,16 | 5.6,38 | 6.158 |
| 13 | 0.7 .11 | 1.6.22 | 2. 2,89 | 2,9,37 | 3.763 | 4.3.65 | 4.9,47 | 5.6,85 | 6. 219 |
| 14 | 0.710 | 1.6 .21 | 2.2,90 | 2.941 | 3.7 .74 | 4. 3,83 | 4.9,73 | 5.7 .25 | 6.271 |
| 15 | 0.7 .09 | 1.6,20 | 2. 291 | 2.945 | 3.7,84 | 4.3,98 | 4.9,96 | 5.7 .59 | $6.3,16$ |
| 16 | 0.7,08 | 1.6,20 | 2. 2,92 | 2.9,48 | 3.792 | 4.4 .12 | 5, 0.15 | 5.789 | 6.354 |
| 17 | 0.7 .07 | 1.6,19 | 2. 2,92 | 2.9,51 | 3.7,99 | 4.4,23 | $5.0,33$ | 5.8,15 | $6.3,88$ |
| 18 | 0.7 .06 | 1.6,19 | 2. 2,93 | 2.9 .54 | 3.8 .06 | 4.4,34 | 5.0.48 | 5.8,38 | 6. 4,18 |
| 19 | 0.7 .05 | 1.6,18 | 2. 293 | 2.9,56 | 3.8,11 | 4.4.43 | 5, 0,61 | 5.8.58 | 6.4,45 |
| 20 | 0.705 | 1.6.18 | 2. 2,94 | 2.9,58 | 3.8,16 | 4.4.51 | 5. 0,74 | 5.8,77 | 6.4,69 |
| 21 | 0.7 .04 | 1.6 .17 | 2. 2,94 | 2.9,60 | 3.8,21 | 4.4.59 | 5.0,85 | 5.8,93 | 6.4,91 |
| 22 | 0.7 .04 | 1.6.17 | 2. 2,95 | 2.961 | 3.8,25 | 4.4,66 | 5.0.95 | 5.9,08 | 6.5,10 |
| 23 | $0.7,03$ | 1.6.16 | 2. 2,95 | 2.963 | 3.8.29 | 4.4,72 | 5.104 | 5.9,22 | 6.5,28 |
| 24 | 0.703 | 1.6 .16 | 2. 2,95 | 2.9,64 | 3.8 .33 | 4.4,78 | 5.1,12 | 5.9,35 | 6.5.44 |
| 25 | 0.7 .02 | 1.616 | 2. 2.96 | 2.966 | 3.8 .36 | 4.4 .83 | 5.1,20 | 5.9,46 | 6.5.59 |
| 26 | 0.702 | 1.616 | 2.296 | 2.967 |  |  |  |  |  |
| 27 | 0.7 .02 | 1.6 .15 | $2.2,96$ | 2.968 | 3.8,39 | $4 \cdot 4,88$ $4.4,92$ | 5.1.27 | $5 \cdot 9,57$ 50,966 | $6 \cdot 5,73$ 6.5 .86 |
| 28 | 0.701 | 1.6.15 | 2. 2,96 | 2.9,69 | 3.8 .44 | 4.4,96 | 5.1.39 | 5.9,75 | 6.5,98 |
| 29 | 0.7 .01 | 1.6.15 | 2. 2,97 | 070 | 3.847 | 4. 5,00 | 5.1,45 | 5.9,84 | 6.6,09 |
| 30 | 0.701 | 1.6.15 | 2.297 | 2.9,71 | 3.8,49 | 4.5,04 | 5.150 | 5.9,92 | 6.6.19 |
| 32 | 0.7 .00 | 1.6.14 | 2.2,97 | 2.9,72 | 3.8.53 | 4, 5,10 | 5.159 | 6. 0.06 |  |
| 34 | 0.7 .00 | 1.6 .14 | 2.2,97 | $2.9,74$ | 3.8 .56 | 4.5,16 | 5.168 | $6.0,18$ | 6.6.54 |
| 36 | 0.7 .00 | 1.614 | 2.298 | 2.9,75 | 3.8 .59 | 4.5,21 | 5.1,75 | $6.0,30$ | 6.6,68 |
| 38 | 0.699 | 1.6,14 | 2.298 | 2.9.76 | 3.8.62 | 4.5,25 | 5.1.82 | 6.0,39 | 6.6,81 |
| 40 | 0.6,99 | 1.6 .13 | 2. 2,98 | 2.9,77 | 3.8 .65 | 4. 5.29 | 5.1 .88 | 6. 0.48 | 6.6,92 |
| 42 | 0.6 .99 | 1.6 .13 | 2. 2.98 | 2.9,78 | 3.8 .67 | 4. 5,33 | 5.193 | 6. 0.56 |  |
| 44 | $0.6,98$ | 1.6,13 | 2. 2,99 | 2.9,79 | 3.8 .69 | 4.5,36 | 5.1.98 | $6.0,64$ | $6 \cdot 7,12$ |
| 46 | $0.6,98$ | 1.6,13 | 2.299 | 2.9,79 | 3.8,71 | 4.5,39 | 5. 2,02 | 6.0,70 | 6.7 .21 |
| 48 | 0.6 .98 | 1.6.13 | 2. 2,99 | 2.980 | 3.8.73 | 4.542 | 5. 206 | 6. 0,76 | 6.7 .29 |
| 50 | 0.698 | 1.6 .13 | 2. 2.99 | 2.9,81 | 3.8 .74 | 4. 5,45 | 5.2,10 | 6.0,82 | 6.7 .36 |
| 55 | 0.697 | 1.612 | 2. 2,99 | 2.9,82 | 3.8.78 | 4. 5,50 | 5. 2,18 | $6.0,94$ | 6.7.52 |
| 60 | 0.6 .97 | 1.6,12 | 2. 3,00 | 2.9.83 | 3.8,81 | 4. 5.55 | 5.225 | 6.104 | 6.7.65 |
| 65 | 0.6 .97 | 1.6.12 | 2. 3,00 | 2.9,84 | 3.8.83 | 4.5,59 | 5.231 | 6.1113 | 6.7,76 |
| 70 | 0.6.96 | 1.612 | 2. 3,00 | 2.9,85 | 3.8 .85 | 4.5.62 | 5.2,35 | 6.120 | 6.7,86 |
| 75 | 0.6 .96 | 1.6,12 | 2. 3.00 | 2.9,86 | 3.8,87 | 4.5,65 | 5.2 .40 | 6.127 | 6.7,94 |
| 80 | 0.6.96 | 1.6.11 | 2.3,00 | 2.986 | 3.8.89 | 4.567 | 5. 2.43 | 6.132 | 6. 8,01 |
| 90 | 0,6,96 | 1.6.11 | 2. 3.01 | 2.9,87 | 3.8 .91 | 4.5,72 | 5.249 | 6.141 | $6.8,13$ |
| 100 | 0.695 | 1.6,11 | 2. 3.01 | 2.9,88 | 3.8 .93 | 4.5,75 | 5.2,54 | 6.149 | $6.8,22$ |
| 120 | 0.695 | 1. 6.11 | 2. 3.01 | 2.9,90 | 3.8,96 | 4.5,80 | 5. 2,62 | $6.1,60$ | $6.8,37$ |
| 140 | $0.6,95$ | 1.6.11 | 2. 3.01 | 2.9,90 | 3.8.99 | 4.5,84 | 5.2,67 | 6.1.68 | 6.8,47 |
| 160 | 0.6 .95 | 1.6,10 | 2.3,01 | 2.9,91 | 3.9 .00 | 4.5886 | 5.271 | 6.174 | 6. 8,55 |
| 180 | 0.6,94 | 1.6,10 | 2. 3.02 | 2.9,92 | 3.9,02 | 4.5,88 | 5.2,74 | 6.178 | $6.8,61$ |
| 200 | 0.694 | 1.6,10 | 2. 3,02 | 2.992 | 3.903 | 4.5,90 | 5.2,76 | 6.182 | 6. 8,65 |
| 300 | $0.6,94$ | 1.6,10 | $2 \cdot 3,02$ | 2.9,93 | 3.9 .06 | 4-5,95 | 5.284 | $6.1,93$ | 6.8,79 |
| 500 | 0.6 .94 | 1.6,10 | $2.3,02$ | 2.9,94 | 3.9 .08 | 4.5,99 | 5.290 | 6.201 | 6.8 .91 |
| $\infty$ | 0.6 .931 | 1.6094 | 2. 3,026 | 2.9957 | 3.9,120 | 4.65052 | 5.2,983 | 6.2146 | 6.9,078 |

Since $24.14>2.971$ reject $H_{0}$.

There is a mean direction of 360 (or 0 ) degrees in the principal azimuths of the Andean villages (Rayleigh $z_{24.14}, p<0.001$ ).

## Analyzing Serial (Monthly) Data as a Circular Distribution

Although serial data can be analyzed using time series, it can also be examined using directional statistics. Remember that both time and date data are measured on a circle and can be converted to angular measurements.

| Chuzmiza, Chile Precipitation Data (2000-2017) | Year |  | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2000 | 49 | 23 | 8 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2001 | 48 | 241 | 165 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2002 | 14 | 68 | 52 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 |
|  | 2003 | 9 | 0 | 11 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 |
|  | 2004 | 6 | 61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2005 | 66 | 56 | 2 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 |
|  | 2006 | 67 | 104 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2007 | 9 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2008 | 146 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2008 | 146 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2009 | 2 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2010 | 0 | 3 | 0 | 8 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2011 | 32 | 188 | 0 | 0 | 5 | 0 | 26 | 0 | 0 | 0 | 0 | 28 |
|  | 2012 | 131 | 176 | 152 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 |
|  | 2013 | 22 | 63 | 6 | 0 | 14 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2014 | 61 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2015 | 5 | 49 | 61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 2016 | 0 | 45 | 0 | 3 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 3 |
|  | 2017 | 81 | 80 | 83 | 0 | 3 | 8 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Total | 892 | 1284 | 540 | 17 | 31 | 13 | 48 | 0 | 12 | 0 | 0 |  |

$$
\text { Angle }=\frac{360 \text { degrees }}{12 \text { months }}=30^{\circ} \text { group interval }
$$

| Month | Total <br> Precip | Angle |
| :---: | :---: | :---: |
| Jan | 892 | 30 |
| Feb | 1284 | 60 |
| Mar | 540 | 90 |
| Apr | 17 | 120 |
| May | 31 | 150 |
| Jun | 13 | 180 |
| Jul | 48 | 210 |
| Aug | 0 | 240 |
| Sep | 12 | 270 |
| Oct | 0 | 300 |
| Nov | 0 | 330 |
| Dec | 57 | 360 |

$$
X=\frac{\sum f_{i}\left(\cos a_{i}\right)}{n} \quad Y=\frac{\sum f_{i}\left(\sin a_{i}\right)}{n} \quad r_{c}=c r \quad c=\frac{\frac{41}{360^{\circ}}}{\sin \left(\frac{d}{2}\right)}
$$

Where $r_{c}$ is the corrected $r, c$ is the correction factor, $n$ is the frequency sum, and $d$ is the group interval.

|  | Month | Total Precip ( $\mathrm{f}_{\mathrm{i}}$ ) | Angle ( $\mathrm{a}_{\mathrm{i}}$ ) | X | Y |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $X_{J a n}=\frac{(892)(\cos 30)}{2894}=0.2669$ | Jan | 892 | 30 | 0.2669 | 0.1541 |
|  | Feb | 1284 | 60 | 0.2218 | 0.3842 |
|  | Mar | 540 | 90 | 0.0000 | 0.0292 |
|  | Apr | 17 | 120 | -0.0029 | 0.0051 |
| $Y_{J a n}=\frac{(892)(\sin 30)}{2894}=0.1541$ | May | 31 | 150 | -0.0093 | 0.0054 |
|  | Jun | 13 | 180 | 0.0045 | 0.0000 |
|  | Jul | 48 | 210 | -0.0144 | -0.0083 |
|  | Aug | 0 | 240 | 0.0000 | 0.0000 |
|  | Sep | 12 | 270 | 0.0000 | -0.0041 |
|  | Oct | 0 | 300 | 0.0000 | 0.0000 |
|  | Nov | 0 | 330 | 0.0000 | 0.0000 |
|  | Dec | 57 | 360 | 0.0197 | 0.0000 |
|  | $\Sigma$ | $\mathrm{n}=2894$ | --- | 0.4863 | 0.5656 |

$$
r=\sqrt{\left(0.4863^{2}\right)\left(0.5656^{2}\right)}=0.2451
$$

Total

|  | Total |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Month | Precip | Angle | $\mathbf{X}$ | $\mathbf{Y}$ |
| Jan | 892 | 30 | 0.2669 | 0.1541 |
| Feb | 1284 | 60 | 0.2218 | 0.3842 |
| Mar | 540 | 90 | 0.0000 | 0.0292 |
| Apr | 17 | 120 | -0.0029 | 0.0051 |
| May | 31 | 150 | -0.0093 | 0.0054 |
| Jun | 13 | 180 | 0.0045 | 0.0000 |
| Jul | 48 | 210 | -0.0144 | -0.0083 |
| Aug | 0 | 240 | 0.0000 | 0.0000 |
| Sep | 12 | 270 | 0.0000 | -0.0041 |
| Oct | 0 | 300 | 0.0000 | 0.0000 |
| Nov | 0 | 330 | 0.0000 | 0.0000 |
| Dec | 57 | 360 | 0.0197 | 0.0000 |
| $\Sigma$ | 2894 | --- | 0.4863 | 0.5656 |

$$
\begin{gathered}
c=\frac{\frac{12 \Pi}{360^{\circ}}}{\sin \left(\frac{12}{2}\right)}=1.0021 \\
r_{c}=0.2451(1.0021)=0.2456 \\
\cos \bar{a}=\frac{0.4863}{0.2456}=1.9800 \\
\sin \bar{a}=\frac{0.5656}{0.2456}=2.3029 \\
\theta_{r}=\arctan \left(\frac{2.3029}{1.9800}\right)=49.31
\end{gathered}
$$

Since the sin and cos are + , + , we read the degrees directly: $49.31^{\circ}$.
$49.31=\frac{(360)(x)}{365}=\frac{360}{365}(49.31)=48.6$ or 49


Therefore the mean precipitation date is the $49^{\text {th }}$ day of the year, or February $18^{\text {th }}$.


## Hypothesis Testing: Uniformity

We can also test the hypothesis that the azimuths are not uniformly distributed (occur equally around the compass).
$H_{0}$ : The distribution of slope aspects is not significantly different than uniform around the compass.
$H_{a}$ : The distribution of slope aspects is significantly different than uniform around the compass.


Observed Distribution


Uniform Distribution

To test this hypothesis we can use the ratio of the observed slope aspects to the expected (uniform) slope aspects and $\chi^{2}$.

- If the sample size is reasonable large (>30) this technique works well.
- If possible, group the data such that no group has less than 4 observations.
- Sometimes grouping in this way is not possible.

First we need to calculate the expected values. Since we are using a uniform distribution, the expected values are:

$$
\hat{f}_{i}=\frac{\text { Sample Size }}{\text { Categories }}
$$

and all expected values for each group will be the same.

We then test the $X^{2}$ statistic, which is calculated as:

$$
\chi^{2}=\sum \frac{\left(f_{i}-\hat{f}_{i}\right)^{2}}{\hat{f}_{i}}
$$

Charcoal hearth platforms on Mt. Newman, Michaux State Forest


Ho: The distribution of platforms is not different than uniform. Ha : The distribution of platforms is different than uniform.

$$
\begin{aligned}
& \begin{array}{rcc} 
& f_{i} & \hat{f}_{i} \\
\text { North } & 4 & 7.25 \\
\text { East } & 14 & 7.25 \\
\text { South } & 9 & 7.25 \\
\text { West } & 5 & 7.25 \\
\mathrm{n}= & 29 &
\end{array} \\
& \chi^{2}=\frac{(4-7.25)^{2}}{7.25}+\frac{(14-7.25)^{2}}{7.25}+\frac{(9-7.25)^{2}}{7.25}+\frac{(5-7.25)^{2}}{7.25} \\
& \chi^{2}=1.46+6.28+0.42+0.70 \\
& \chi^{2}=8.86 \\
& d f=k-1=4-1=3 \\
& \chi_{\text {Critical }}^{2}=7.815
\end{aligned}
$$

|  | .995 | .975 | . 9 | . 5 | . 1 | . 05 | . 025 | . 01 | . 005 | 00 | $\alpha / v$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.000 | 0.000 | 0.016 | 0.455 | 2.706 | 3.841 | 5.024 | 6.635 | 7.879 | 10.828 | 1 |
| 2 | 0.010 | 0.051 | 0.211 | 1.386 | 4.605 | 5001 | 7.378 | 9.210 | 10.597 | 13.816 | 2 |
| 3 | 0.072 | 0.216 | 0.584 | 2.366 | 6.251 | 7.815 | 9.348 | 11.345 | 12.838 | 16.266 | 3 |
| 4 | 0.207 | 0.484 | 1.064 | 3.357 | 7.779 | 9.488 | 11.143 | 13.277 | 14.860 | 18.467 | 4 |
| 5 | 0.412 | 0.831 | 1.610 | 4.351 | 9.236 | 11.070 | 12.832 | 15.086 | 16.750 | 20.515 | 5 |
| 6 | 0.676 | 1.237 | 2.204 | 5.348 | 10.645 | 12.592 | 14.449 | 16.812 | 18.548 | 22.458 | 6 |
| 7 | 0.989 | 1.690 | 2.833 | 6.346 | 12.017 | 14.067 | 16.013 | 18.475 | 20.278 | 24.322 | 7 |
| 8 | 1.344 | 2.180 | 3.490 | 7.344 | 13.362 | 15.507 | 17.535 | 20.090 | 21.955 | 26.124 | 8 |
| 9 | 1.735 | 2.700 | 4.168 | 8.343 | 14.684 | 16.919 | 19.023 | 21.666 | 23.589 | 27.877 | 9 |
| 10 | 2.156 | 3.247 | 4.865 | 9.342 | 15.987 | 18.307 | 20.483 | 23.209 | 25.188 | 29.588 | 0 |
| 11 | 2.603 | 3.816 | 5.578 | 10.341 | 17.275 | 19.675 | 21.920 | 24.725 | 26.757 | 31.264 | 11 |
| 12 | 3.074 | 4.404 | 6.304 | 11.340 | 18.549 | 21.026 | 23.337 | 26.217 | 28.300 | 32.910 | 12 |
| 13 | 3.565 | 5.009 | 7.042 | 12.340 | 19.812 | 22.362 | 24.736 | 27.688 | 29.819 | 34.528 | 13 |
| 14 | 4.075 | 5.629 | 7.790 | 13.339 | 21.064 | 23.685 | 26.119 | 29.141 | 31.319 | 36.123 | 14 |
| 15 | 4.601 | 6.262 | 8.547 | 14.339 | 22.307 | 24.996 | 27.488 | 30.578 | 32.801 | 37.697 | 15 |
| 16 | 5.142 | 6.908 | 9.312 | 15.338 | 23.542 | 26.296 | 28.845 | 32.000 | 34.267 | 39.252 | 6 |
| 17 | 5.697 | 7.564 | 10.085 | 16.338 | 24.769 | 27.587 | 30.191 | 33.409 | 35.718 | 40.790 | 17 |
| 18 | 6.265 | 8.231 | 10.865 | 17.338 | 25.989 | 28.869 | 31.526 | 34.805 | 37.156 | 42.312 | 18 |
| 19 | 6.844 | 8.907 | 11.651 | 18.338 | 27.204 | 30.144 | 32.852 | 36.191 | 38.582 | 43.820 | 19 |
| 20 | 7.434 | 9.591 | 12.443 | 19.337 | 28.412 | 31.410 | 34.170 | 37.566 | 39.997 | 45.315 | 20 |
| 21 | 8.034 | 10.283 | 13.240 | 20.337 | 29.615 | 32.670 | 35.479 | 38.932 | 41.401 | 46.797 | 21 |
| 22 | 8.643 | 10.982 | 14.042 | 21.337 | 30.813 | 33.924 | 36.781 | 40.289 | 42.796 | 48.268 | 22 |
| 23 | 9.260 | 11.688 | 14.848 | 22.337 | 32.007 | 35.172 | 38.076 | 41.638 | 44.181 | 49.728 | 23 |
| 24 | 9.886 | 12.401 | 15.659 | 23.337 | 33.196 | 36.415 | 39.364 | 42.980 | 45.558 | 51.179 | 24 |
| 25 | 10.520 | 13.120 | 16.473 | 24.337 | 34.382 | 37.652 | 40.646 | 44.314 | 46.928 | 52.620 | 25 |
| 26 | 11.160 | 13.844 | 17.292 | 25.336 | 35.563 | 38.885 | 41.923 | 45.642 | 48.290 | 54.052 | 26 |
| 27 | 11.808 | 14.573 | 18.114 | 26.336 | 36.741 | 40.113 | 43.194 | 46.963 | 49.645 | 55.476 | 27 |
| 28 | 12.461 | 15.308 | 18.939 | 27.336 | 37.916 | 41.337 | 44.461 | 48.278 | 50.993 | 56.892 | 28 |
| 29 | 13.121 | 16.047 | 19.768 | 28.336 | 39.088 | 42.557 | 45.722 | 49.588 | 52.336 | 58.301 | 29 |
| 30 | 13.787 | 16.791 | 20.599 | 29.336 | 40.256 | 43.773 | 46.979 | 50.892 | 53.672 | 59.703 | 30 |
| 31 | 14.458 | 17.539 | 21.434 | 30.336 | 41.422 | 44.985 | 48.232 | 52.191 | 55.003 | 61.098 | 31 |
| 32 | 15.134 | 18.291 | 22.271 | 31.336 | 42.585 | 46.194 | 49.480 | 53.486 | 56.329 | 62.487 | 32 |
| 33 | 15.815 | 19.047 | 23.110 | 32.336 | 43.745 | 47.400 | 50.725 | 54.776 | 57.649 | 63.870 | 33 |
| 34 | 16.501 | 19.806 | 23.952 | 33.336 | 44.903 | 48.602 | 51.966 | 56.061 | 58.964 | 65.247 | 34 |
| 35 | 17.192 | 20.569 | 24.797 | 34.336 | 46.059 | 49.802 | 53.203 | 57.342 | 60.275 | 66.619 | 35 |
| 36 | 17.887 | 21.336 | 25.643 | 35.336 | 47.212 | 50.998 | 54.437 | 58.619 | 61.582 | 67.985 | 36 |
| 37 | 18.586 | 22.106 | 26.492 | 36.335 | 48.363 | 52.192 | 55.668 | 59.892 | 62.884 | 69.346 | 37 |
| 38 | 19.289 | 22.878 | 27.343 | 37.335 | 49.513 | 53.384 | 56.896 | 61.162 | 64.182 | 70.703 | 38 |
| 39 | 19.996 | 23.654 | 28.196 | 38.335 | 50.660 | 54.572 | 58.120 | 62.428 | 65.476 | 72.055 | 39 |
| 40 | 20.707 | 24.433 | 29.051 | 39.335 | 51.805 | 55.758 | 59.342 | 63.691 | 66.766 | 73.402 | 40 |
| 41 | 21.421 | 25.215 | 29.907 | 40.335 | 52.949 | 56.942 | 60.561 | 64.950 | 68.053 | 74.745 | 41 |
| 42 | 22.138 | 25.999 | 30.765 | 41.335 | 54.090 | 58.124 | 61.777 | 66.206 | 69.336 | 76.084 | 42 |
| 43 | 22.859 | 26.785 | 31.625 | 42.335 | 55.230 | 59.304 | 62.990 | 67.459 | 70.616 | 77.419 | 43 |
| 44 | 23.584 | 27.575 | 32.487 | 43.335 | 56.369 | 60.481 | 64.202 | 68.710 | 71.893 | 78.750 | 44 |
| 45 | 24.311 | 28.366 | 33.350 | 44.335 | 57.505 | 61.656 | 65.410 | 69.957 | 73.166 | 80.077 | 45 |
| 46 | 25.042 | 29.160 | 34.215 | 45.335 | 58.641 | 62.830 | 66.617 | 71.201 | 74.437 | 81.400 | 46 |
| 47 | 25.775 | 29.956 | 35.081 | 46.335 | 59.774 | 64.001 | 67.821 | 72.443 | 75.704 | 82.720 | 47 |
| 48 | 26.511 | 30.755 | 35.949 | 47.335 | 60.907 | 65.171 | 69.023 | 73.683 | 76.969 | 84.037 | 48 |
| 49 | 27.249 | 31.555 | 36.818 | 48.335 | 62.038 | 66.339 | 70.222 | 74.919 | 78.231 | 85.351 | 49 |
| 50 | 27.991 | 32.357 | 37.689 | 49.335 | 63.167 | 67.505 | 71.420 | 76.154 | 79.490 | 86.661 | 50 |

Since $8.86>7.815$, reject $H_{o}$.
The distribution of charcoal hearth platform aspects is not uniform around Mount Newman ( $\mathrm{X}^{2}{ }_{8.86}, 0.05>\mathrm{p}>0.025$ ).

## Two-Sample Hypothesis Testing

We can test the hypothesis that two sets of azimuths are not significantly different in a procedure similar to the MannWhitney U test called Watson's $U^{2}$ test.
$H_{0}$ : The two groups of principal azimuths are not significantly different.
$H_{a}$ : The two groups of principal azimuths are significantly different.

## Watson's U2 test equation:

$$
\begin{aligned}
& U^{2}=\frac{n_{1} n_{2}}{N^{2}}\left[\sum d_{k}^{2}-\frac{\left(\sum d_{k}\right)^{2}}{N}\right] \\
& \text { where } \\
& N=n_{1}+n_{2}
\end{aligned}
$$

- First the data are ranked, smallest to largest.
- $\mathrm{n}_{1}$ and $\mathrm{n}_{2}$ are the group sample sizes.
- The expected frequency ( $\mathrm{i} / \mathrm{n}_{1}$ and $\mathrm{j} / \mathrm{n}_{2}$ ) are then calculated.


## Tree Throws near Corls Ridge,

 Michaux State Forest
$\xrightarrow{73}$


Are these two groups of tree throws on opposite sides of the ridge likely from the same wind event?

Ho: The angles of the two groups are not different.
Ha: The angles of the two groups are different.

Rank all angles


Group A

| i | $\mathrm{a} 1_{\mathrm{i}}(\mathrm{deg})$ | $\mathrm{i} / \mathrm{n}_{1}$ | j | $\mathrm{a} 2_{\mathrm{i}}(\mathrm{deg})$ | $\mathrm{j} / \mathrm{n}_{2}$ | $\mathrm{~d}_{\mathrm{k}}=\mathrm{i} / \mathrm{n}_{1}-\mathrm{j} / \mathrm{n}_{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 55 | 0.1429 |  | $\mathrm{~d}_{\mathrm{k}}$ |  |  |  |
| 2 | 57 | 0.2857 |  |  | 0.0000 | 0.1429 | 0.0204 |
| 3 | 60 | 0.4286 |  |  | 0.0000 | 0.2857 | 0.0816 |
| 4 | 63 | 0.5714 |  |  | 0.0000 | 0.4286 | 0.1837 |
| 5 | 64 | 0.7143 |  |  | 0.0000 | 0.5714 | 0.3265 |
|  |  | 0.7143 | 1 | 65 | 0.1667 | 0.7143 | 0.5102 |
| 6 | 66 | 0.8571 |  |  | 0.1667 | 0.6976 | 0.2999 |
| 7 | 67 | 1.0000 | 2 | 67 | 0.3333 | 0.6667 | 0.4767 |
|  |  | 1.0000 | 3 | 68 | 0.5000 | 0.5000 | 0.2500 |
|  |  | 1.0000 | 4 | 70 | 0.6667 | 0.3333 | 0.1111 |
|  |  | 1.0000 | 5 | 72 | 0.8333 | 0.1667 | 0.0278 |
|  |  | 1.0000 | 6 | 73 | 1.0000 | 0.0000 | 0.0000 |

$$
n_{a 1}=7 \quad n_{a 2}=6 \quad \sum d_{k}=5.0476 \quad \sum d_{k}^{2}=2.7324
$$

$$
U^{2}=\frac{(6)(7)}{42^{2}}\left[2.7324-\frac{(5.0476)^{2}}{42}\right]
$$

$$
U^{2}=\frac{n_{1} n_{2}}{N^{2}}\left[\sum d_{k}^{2}-\frac{\left(\sum d_{k}\right)^{2}}{N}\right]
$$

$$
U^{2}=0.0238(2.7324-0.6066)
$$

$$
U^{2}=0.0506
$$

Critical Values for the Watson $\mathrm{U}^{2}$ Test (cont.)
Taken from Zar, 1981 Table B. 35


Since $0.0506<0.1941$ accept $H_{0}$.
The two groups of are not significantly different $\left(U^{2}{ }_{0.0506}, \mathrm{p}>\right.$ $0.50)$.

